



Force Engineering & Testing Inc.

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Humble, Texas 77338
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Project Number : 13-0459T-08G-I

Test Report Date : March 3, 2009

Test Material : 8" x 2.5" ZEE w/ Tophat

Test Procedure : AISI Uplift Load Base Test

Test Location : Force Engineering & Testing Inc.
19530 Ramblewood Drive
Humble, Texas 77338

Miami Dade County Lab Certification No: 05-1122.13

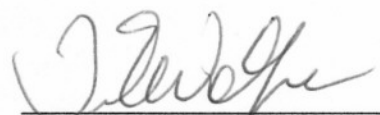
14 GA. REG STRENGTH TOPHAT UPLIFT TEST

Report Prepared by:



Brandon Jasek, P.E.

Report Reviewed by:



Terrence E. Wolfe, P.E.

Project Number : 13-0459T-08G-I

PURPOSE:

The purpose of this test was to analyze the bracing effects on the purlins that the Tophat adds to a through fastened panel system when subjected to a uplift load.

TEST DATES:

December - January 2009

TEST ASSEMBLY:

Panel & Purlin Manufacturer

Manufacturer: Whirlwind Steel Buildings, Inc.
8234 Hansen Road
Houston, TX 77075

Roof Panel: 26 Ga. Super Span X, 36" Coverage, 1 1/4" tall Corrugations.

Panel Fastener: #12-14 x 1" HWH @ 12"-12"-12" Fastener Pattern
1/4-14 x 7/8" Lap Tek @ 20" O.C. in panel side lap

Panel Length: 7'-0"

Purlin: 8" x 2.5" ZEE 16 Ga.

Purlin Length: 25'-7 1/2", Span = 25'-0"

Tophat Manufacturer

Manufacturer: TopHat Framing Systems
8660 Lambright
Houston, TX 77075

Tophat: 14 Ga. Regular Strength, 3 1/2" Tall Hat section w/ R Panel punch out pattern, 0.072" Material Thickness, Fy = 50.6 ksi (Per Tensile Test See Appendix)

Tophat Fastener: (2) #12-14 x 1-1/4" HWH per foot

Tophat Length: 25'-0", No Splice

TESTING APPARATUS:

High Pressure Blower: New York Blower, 15 hp, 900 cfm.

Test Chamber: 26' x 8' steel chamber.

Mounting Frame: W8x10 Steel Beams

Pressure Indicator: Heise Digital Pressure Indicator Model #901B, (+/-) 300-psf range, with max./min. hold features.

Deflection Indicators: aluminum rulers calibrated to 1/64".

INTRODUCTION:

The purpose of this test series was to obtain the moment reduction factor used in determining the nominal flexural strength of a purlin in negative bending supporting a through fastened panel system with a tophat added. The moment reduction factor reflects the ability of existing through fastened panel system with the added tophat to provide lateral and torsional bracing to the purlins to which it is attached. This test is based on the base test procedure provided by the 1996 AISI COLD-FORMED STEEL SPECIFICATION SUPPLEMENT NO. 1 APPENDIX A, JULY 30, 1999. This publication contains all variables, definitions, requirements and calculations for The Base Test Method.

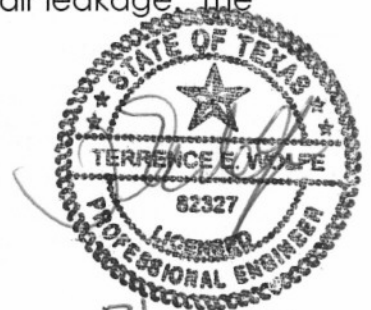
PROCEDURE:

1. The purlins were installed at 5'-0" O.C. upon the steel supporting frames within the pressure chamber simulating recommended field attachment. The purlin clips were slotted on one end to eliminate any centenary forces that might be induced due to the connection.
2. With purlin installation complete, the Super Span X panels were installed.
3. Tophats were then installed over the panels over each purlin.
4. With construction complete, vertical deflection indicators were placed at mid-span of both purlins. A horizontal deflection indicator was placed at the seam nearest to the purlins' mid-span.
5. The test was set at 5 psf and held for minute. After the initial set, a zero reading was taken then positive pressure applied in the increments shown on the data sheets until failure. Deflection readings were taken at each increment and are shown on the data sheets.
6. The above steps were used for three purlins.

RESULTS/CONCLUSIONS:

The 8x2.5 x 16 Ga. Zee failed at 34.85 psf, 33.10 psf and 32.93 psf. The mode of failure was buckling of the purlin bottom stiffener lip in all three test. From the calculation page, the modification factor $R = 0.900$.

Note: During this test, tape and plastic were used to seal against air leakage. The tape and plastic had no restrictive influence on the test.



3/17/09

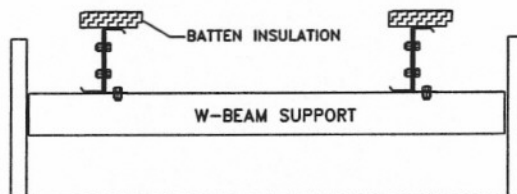
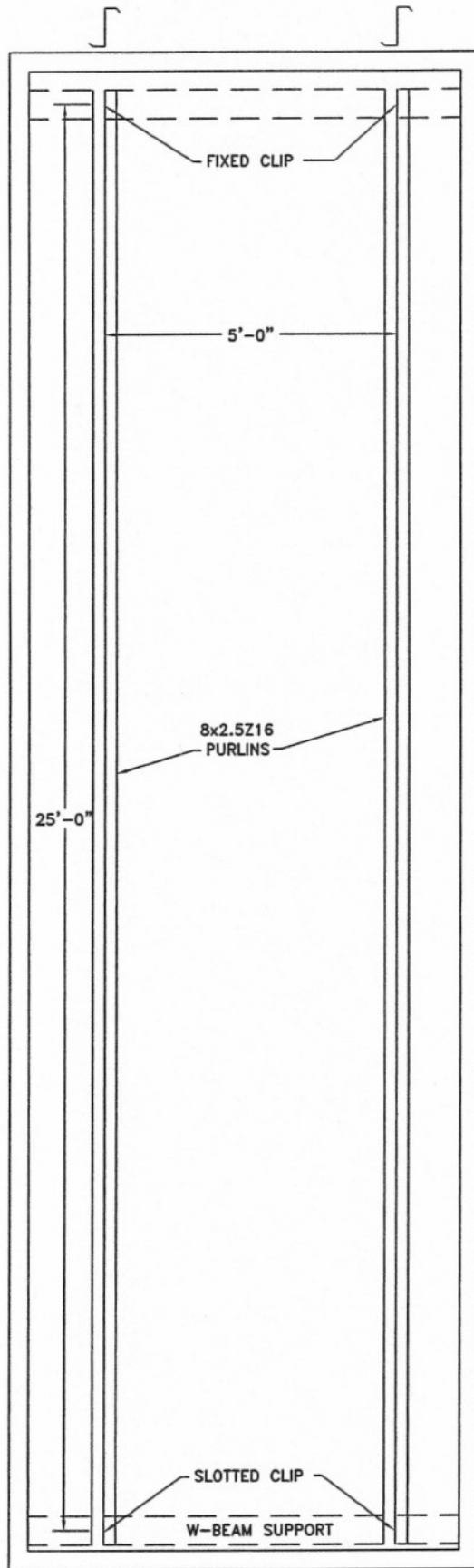
STATEMENT OF INDEPENDENCE:

Force Engineering & Testing, Inc. or any persons employed by them do not have any financial interest in Whirlwind or TopHat Framing Systems.

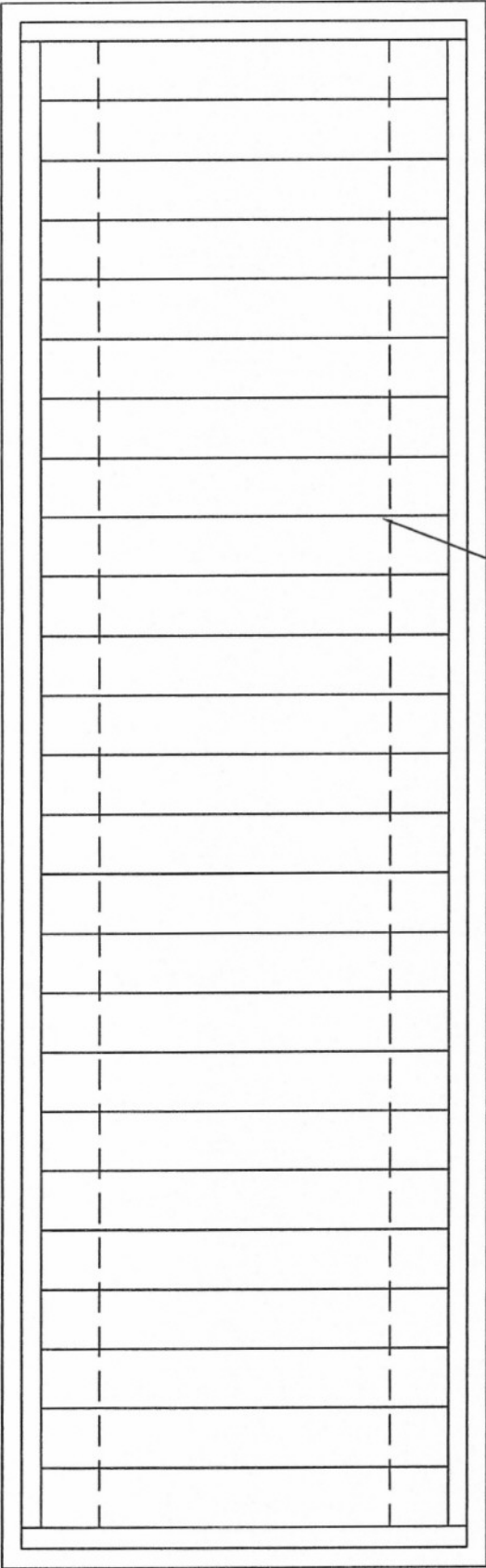
Force Engineering & Testing, Inc. is not owned, operated or controlled by Whirlwind or TopHat Framing Systems.

Appendix

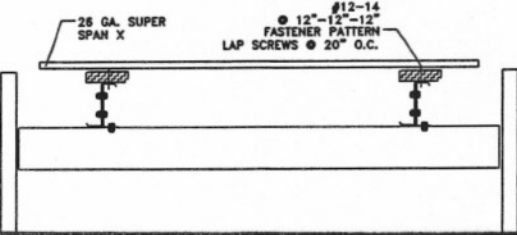
PURLIN LAYOUT



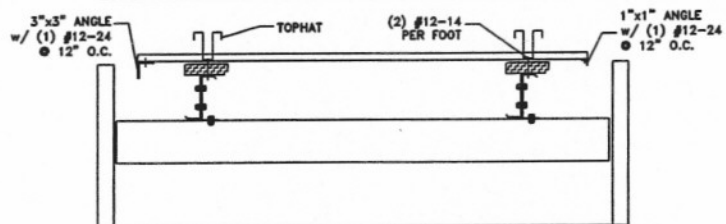
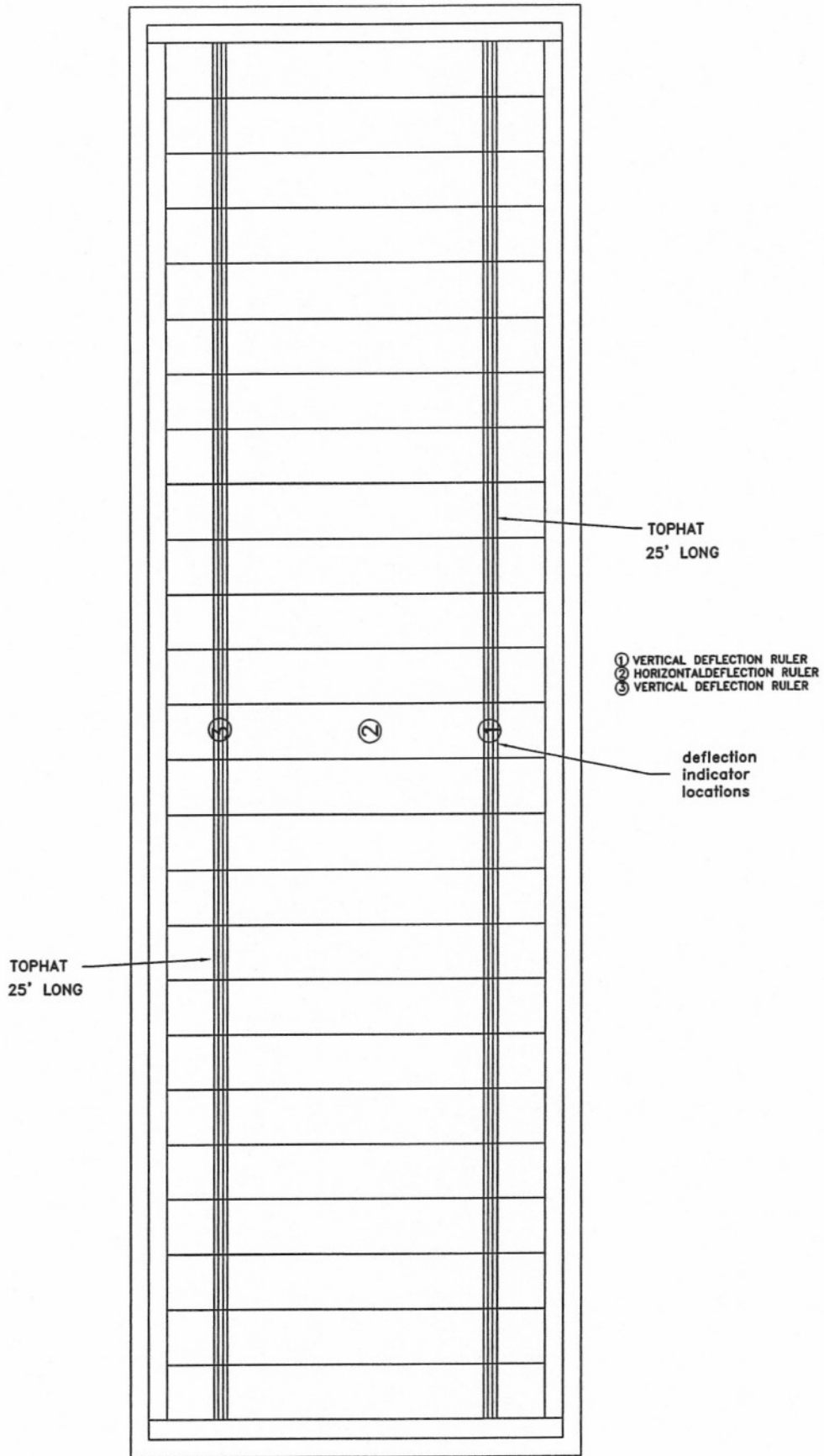
PANEL LAYOUT



26 GA. SUPER SPAN X PANEL



TOPHAT LAYOUT



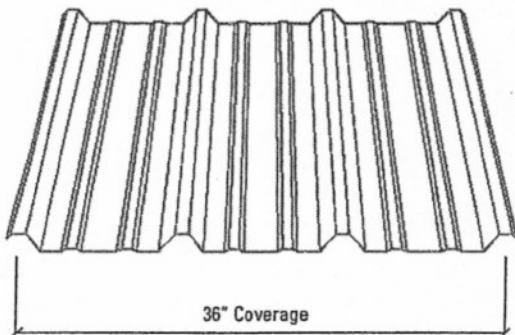
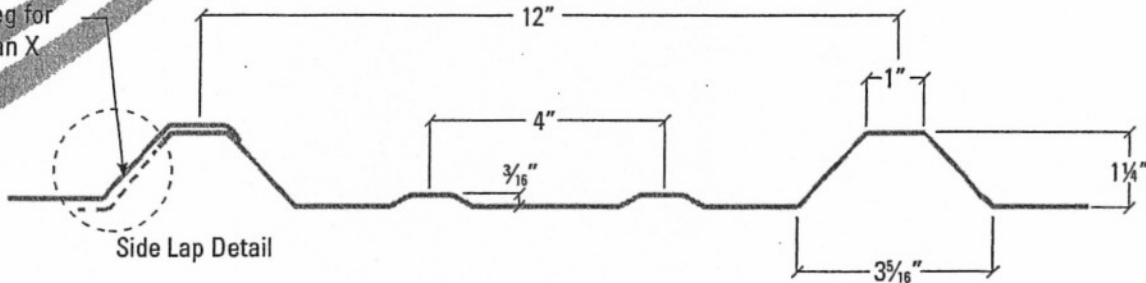


WHIRLWIND BUILDING COMPONENTS
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SUPER SPAN-X

Bearing leg for Super Span X



GAUGE/ THICKNESS	F _y (KSI)	F _b (KSI)	TOP IN COMPRESSION		BOTTOM IN COMPRESSION	
			I _x (In ⁴ -Ft)	M _a (Kip-In/Ft)	I _x (In ⁴ -Ft)	M _a (Kip-In/Ft)
26 (t=.0170")	60*	0.83	0.0370	1.2697	0.0323	1.6610
26 (t=.0176")	60*	0.86	0.0380	1.4057	0.0337	1.7230
24	50	1.09	0.0570	1.7500	0.0467	1.8633

* F_y is 80-ksi reduced to 60-ksi in accordance with the 2001 edition of the North American Specification For Design Of Cold-Formed Steel Structural Members - A2.3.2.

NOTES:

- All section properties are calculated in accordance with the 2001 edition of the North American Specification For Design Of Cold-Formed Steel Structural Members.
- I_x is for deflection determination.
- M_x is allowable bending moment.

MATERIALS

Unless otherwise specified, the exposed surfaces of all panels shall be either clear acrylic coated or factory painted GALVALUME®. GALVALUME® is a zinc-aluminum alloy coating that is applied to the base steel material. Acrylic coated GALVALUME® shall have a Coating Class AZ50 (0.50 ounces (combined total of both sides) per square foot). Factory painted GALVALUME® shall have a minimum Coating Class AZ50 (0.50 ounces (combined total of both sides) per square foot). GALVALUME® coated steel for panels shall conform to ASTM A792, Structural Quality. The 26 gauge panel shall conform to Grade 80 (80 ksi minimum yield strength); the 24 gauge panel shall conform to Grade 50 (50 ksi minimum yield strength). All material shall be ordered to a minimum decimal thickness. Minimum ordered thickness for coated steel products always includes the thickness of the coating.

PAINTED FINISH

All painted GALVALUME® shall be factory coated by a firm which coats coil products exclusively. The coater shall be responsible for ensuring color consistency, paint film hardness, and paint film thickness. Each side of the GALVALUME® will be coated with 0.2 mils baked-on primer before the color coating. The 26 gauge panel shall receive a baked-on silicone polyester finish coat on the exposed side. The 24 gauge panel shall receive a KYNAR 500® Fluoropolymer finish coat on the exposed side. Thickness of the finish coat will be a nominal 1.0 mils (including the primer coat). A baked-on straight polyester wash coat will be applied on the non-exposed side. Thickness of the wash coat will be a nominal 0.5 mils (including the primer coat).

LIMITED MATERIAL WARRANTY

Specific conditions concerning each finish shall be covered in detail on the written warranty issued, on request, with each order. Minimum roof slope - 1/2:12. GALVALUME® panels shall have a twenty-five year limited warranty providing that GALVALUME® panels will not rupture, fail structurally, or perforate within a period twenty-five years after shipment due to exposure to normal atmospheric corrosion. The clear acrylic finish does not carry a warranty. The 26 gauge factory coated GALVALUME® panel shall have a thirty-year limited color finish warranty from peeling and cracking, and a twenty-five year limited color finish warranty from excessive chalking and color change (fading). The 24 gauge factory coated GALVALUME® panel shall have a thirty-year limited color finish warranty from excessive chalking and color change (fading), peeling and cracking. The wash coat does not carry a warranty.

PANELS

Panel coverage will be 36" to the weather. Maximum panel length shall be 40'-0". Where endlaps are required, they shall be a minimum of 4" and shall occur at a purlin. A roof installed as listed in UL Construction No. 167 shall meet the requirements of Underwriters Laboratories standard UL 580 Class 90 for uplift resistance. All installations shall be in accordance with standard industry practices. Before securing, all laps of roof panels shall be sealed with a continuous ribbon of tape sealant. A closure strip shall be installed at the eave. Panels shall be secured to intermediate framing members with sheet metal screws at a maximum spacing of 12" on center. At endlaps, the maximum screw spacing shall be 6" on center. Sheet metal stitch screws at a maximum of 20" on center shall be installed at sidelaps. The panel must not rest on the concrete foundation; the panel must sit 1/8" above the concrete. Panels shall be furnished square cut.

- **UL CONSTRUCTION NO. 167**
- **UL 580 UP-LIFT TESTED CLASS 90 RATED**
- **UL 2218 HAIL IMPACT RESISTANT TESTED**
- **INCLINED: UNLIMITED IMPACT: CLASS 4**
- **FLORIDA PRODUCT APPROVAL FL# 1845.3**

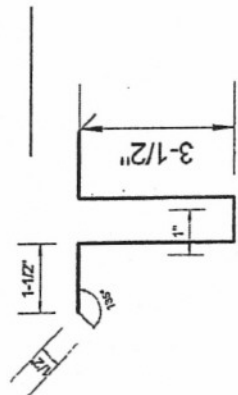
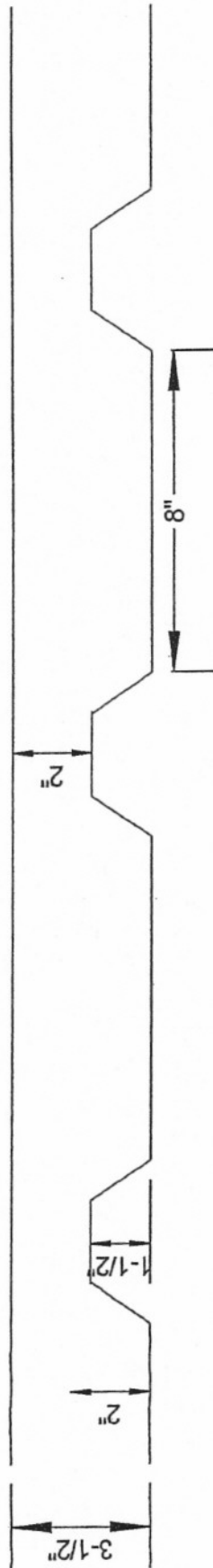
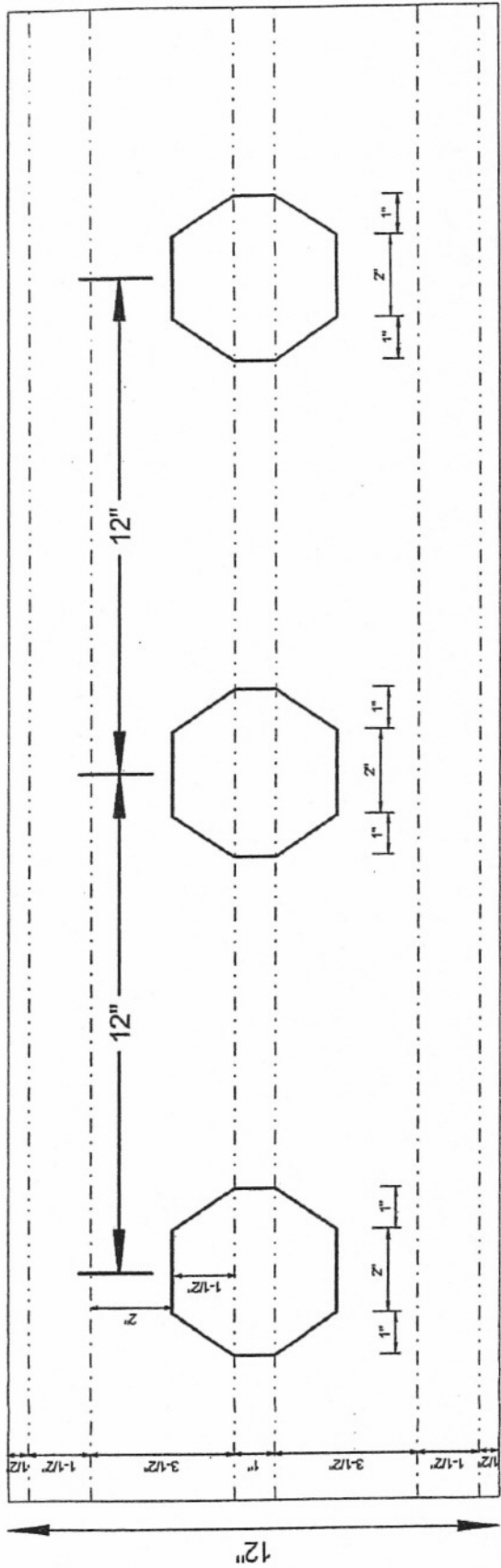
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MECHANICAL
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ISO 9001-2000

CERTIFICATE OF TEST

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CUSTOMER : FORCE ENGINEERING & TESTING INC.
19530 RAMBLEWOOD DR
HUMBLE, TX 77338

8676 TAUB ROAD
Houston, TX 77064
281/469-2609

LAB# : W0901584

DATE : 02/12/09 12:16:02
PO NO :13-0459T-08
SPECIMEN :14RTP

TEST DATA

REDUCED SECTION TENSILE

UTS PSI	YS.2%PSI	%EL	%RA	WIDTH	THICK	AREA IN.
59,500	50,600	34.70	59.40	0.500	0.072	0.036


MTEC Representative

Data Sheets

Calculations

CALCULATIONS

PANEL : 26 Ga. PBR 7'-0" long
 CLIP : NA
 FASTENER : #12-14 x 1-1/4" HWH
 PURLIN : 8x2.5Zee w/ Tophat attached w/ (2) #12-14 every foot
 TOPHAT : 14 Ga. Reg Strength Tophat
 DESCRIPTION : 25'-0" Span Uplift Base Test

#1 12-5-08	8X2.5X16GA. ZEE		
b	purlin flange width	2.125	in.
B	purlin spacing	60.00	in.
d	purlin depth	8.00	in.
t	purlin thickness	0.059	in.
pts	failure load	34.85	psf
pd	weight of the specimen	2.550	psf
s	purlin tributary width	3.500	ft
PI	lateral anchorage force	13.98	lbs/ft
wts	failure load	113.05	lbs/ft
L	purlin span	25.00	ft
Mts	failure moment	105.98	k-in
Set	section modulus of the specimen	1.7152	in ³
Se	section modulus	1.7701	in ³
Fy	design yield strength	57.00	ksi
Fyt	measured yield strength	62.20	ksi
Mn	nominal flexural strength	100.90	k-in
Mnt	flexural strength	106.69	k-in
Rt	modification factor	0.9934	

#2 1-19-09	8X2.5X16GA. ZEE		
b	purlin flange width	2.125	in.
B	purlin spacing	60.00	in.
d	purlin depth	8.00	in.
t	purlin thickness	0.059	in.
pts	failure load	33.10	psf
pd	weight of the specimen	2.550	psf
s	purlin tributary width	3.500	ft
PI	lateral anchorage force	13.32	lbs/ft
wts	failure load	106.93	lbs/ft
L	purlin span	25.00	ft
Mts	failure moment	100.24	k-in
Set	section modulus of the specimen	1.6827	in ³
Se	section modulus	1.7701	in ³
Fy	design yield strength	57.00	ksi
Fyt	measured yield strength	64.80	ksi
Mn	nominal flexural strength	100.90	k-in
Mnt	flexural strength	109.04	k-in
Rt	modification factor	0.9193	

#3 1-23-09	8X2.5X16GA. ZEE		
b	purlin flange width	2.125	in.
B	purlin spacing	60.00	in.
d	purlin depth	8.00	in.
t	purlin thickness	0.059	in.
pts	failure load	32.93	psf
pd	weight of the specimen	2.550	psf
s	purlin tributary width	3.500	ft
PI	lateral anchorage force	13.26	lbs/ft
wts	failure load	106.33	lbs/ft
L	purlin span	25.00	ft
Mts	failure moment	99.68	k-in
Set	section modulus of the specimen	1.6876	in ³
Se	section modulus	1.7701	in ³
Fy	design yield strength	57.00	ksi
Fyt	measured yield strength	64.40	ksi
Mn	nominal flexural strength	100.90	k-in
Mnt	flexural strength	108.68	k-in
Rt	modification factor	0.9172	

AVERAGE Rt	0.943
STANDARD DEVIATION	0.043
Rt min.	0.900
Mnt min.	108.135



Section Inputs

Material: A1011 HSLAS Grade 55/2
 No strength increase from cold work of forming.
 Modulus of Elasticity, E 29500 ksi
 Yield Strength, Fy 57 ksi
 Tensile Strength, Fu 65 ksi
 Warping Constant Override, Cw 0 in⁶
 Torsion Constant Override, J 0 in⁴

Z-Section, Thickness 0.0589 in
 Placement of Part from Origin:
 X to center of gravity 0 in
 Y to center of gravity 0 in

Outside dimensions, Open shape

	Length (in)	Angle (deg)	Radius (in)	Web	k Coef.	Hole Size (in)	Distance (in)
1	0.9410	-50.000	0.25000	None	0.000	0.0000	0.4705
2	2.1250	0.000	0.25000	Single	0.000	0.0000	1.0625
3	8.0000	90.000	0.25000	Zee	0.000	0.0000	4.0000
4	2.3750	0.000	0.25000	Single	0.000	0.0000	1.1875
5	0.9410	-50.000	0.25000	None	0.000	0.0000	0.4705

Fully Braced Strength - 2001 AISI Specification - US (ASD)

Compression		Positive Moment		Positive Moment	
Pao	14942 lb	Maxo	61.130 k-in	Mayo	11.825 k-in
Ae	0.47186 in ²	Ixe	7.2926 in ⁴	Iye	1.0183 in ⁴
		Sxe(t)	1.7910 in ³	Sye(l)	0.3755 in ³
		Sxe(b)	1.8565 in ³	Sye(r)	0.3465 in ³
		Negative Moment		Negative Moment	
		Maxo	60.415 k-in	Mayo	12.367 k-in
		Ixe	7.3990 in ⁴	Iye	1.0370 in ⁴
		Sxe(t)	1.9370 in ³	Sye(l)	0.3718 in ³
		Sxe(b)	1.7701 in ³	Sye(r)	0.3623 in ³
Tension					
Ta	26677 lb				
Shear					
Vay	2463 lb				
Vax	4525 lb				



Section Inputs

Material: [A1011 HSLAS Grade 55/2]
 No strength increase from cold work of forming.
 Modulus of Elasticity, E 29500 ksi
 Yield Strength, Fy 62.2 ksi
 Tensile Strength, Fu 76.7 ksi
 Warping Constant Override, Cw 0 in⁶
 Torsion Constant Override, J 0 in⁴

Z-Section, Thickness 0.059 in
 Placement of Part from Origin:
 X to center of gravity 0 in
 Y to center of gravity 0 in

Outside dimensions, Open shape

	Length (in)	Angle (deg)	Radius (in)	Web	k Coef.	Hole Size (in)	Distance (in)
1	0.9410	-50.000	0.25000	None	0.000	0.0000	0.4705
2	2.1250	0.000	0.25000	Single	0.000	0.0000	1.0625
3	8.0000	90.000	0.25000	Zee	0.000	0.0000	4.0000
4	2.3750	0.000	0.25000	Single	0.000	0.0000	1.1875
5	0.9410	-50.000	0.25000	None	0.000	0.0000	0.4705

Fully Braced Strength - 2001 AISI Specification - US (ASD)

Compression		Positive Moment		Positive Moment	
Pao	15826 lb	Maxo	65.139 k-in	Mayo	12.723 k-in
Ae	0.45800 in ²	Ixe	7.1940 in ⁴	Iye	1.0068 in ⁴
		Sxe(t)	1.7489 in ³	Sye(l)	0.3724 in ³
		Sxe(b)	1.8510 in ³	Sye(r)	0.3416 in ³
		Negative Moment		Negative Moment	
		Maxo	63.884 k-in	Mayo	13.397 k-in
		Ixe	7.2719 in ⁴	Iye	1.0267 in ⁴
		Sxe(t)	1.9338 in ³	Sye(l)	0.3671 in ³
		Sxe(b)	1.7152 in ³	Sye(r)	0.3597 in ³
Shear					
Vay	2476 lb				
Vax	4946 lb				



Section Inputs

Material: [A1011 HSLAS Grade 55/2]
 No strength increase from cold work of forming.
 Modulus of Elasticity, E 29500 ksi
 Yield Strength, Fy 64.8 ksi
 Tensile Strength, Fu 75.6 ksi
 Warping Constant Override, Cw 0 in⁶
 Torsion Constant Override, J 0 in⁴

Z-Section, Thickness 0.059 in
 Placement of Part from Origin:
 X to center of gravity 0 in
 Y to center of gravity 0 in

Outside dimensions, Open shape

	Length (in)	Angle (deg)	Radius (in)	Web	k Coef.	Hole Size (in)	Distance (in)
1	0.9410	-50.000	0.25000	None	0.000	0.0000	0.4705
2	2.1250	0.000	0.25000	Single	0.000	0.0000	1.0625
3	8.0000	90.000	0.25000	Zee	0.000	0.0000	4.0000
4	2.3750	0.000	0.25000	Single	0.000	0.0000	1.1875
5	0.9410	-50.000	0.25000	None	0.000	0.0000	0.4705

Fully Braced Strength - 2001 AISI Specification - US (ASD)

Compression		Positive Moment		Positive Moment	
Pao	16214 lb	Maxo	66.512 k-in	Mayo	13.054 k-in
Ae	0.45040 in ²	Ixe	7.1116 in ⁴	Iye	0.9939 in ⁴
		Sxe(t)	1.7141 in ³	Sye(l)	0.3686 in ³
		Sxe(b)	1.8466 in ³	Sye(r)	0.3364 in ³
		Negative Moment		Negative Moment	
		Maxo	65.293 k-in	Mayo	13.896 k-in
		Ixe	7.1915 in ⁴	Iye	1.0208 in ⁴
		Sxe(t)	1.9300 in ³	Sye(l)	0.3646 in ³
		Sxe(b)	1.6827 in ³	Sye(r)	0.3581 in ³
Tension					
Ta	31079 lb				
Shear					
Vay	2476 lb				
Vax	5152 lb				

Section: 14 Ga. Reg Test 3.sct
 8 x 2.5 Z 16 Gage
 LGSI Library
 Rev. Date: 2/26/2009 10:09:04 AM
 By: Brandon Jasek

Brandon Jasek
 Force Engineering & Testing
 14 Ga. Reg Test 3



Section Inputs

Material: [A1011 HSLAS Grade 55/2]
 No strength increase from cold work of forming.
 Modulus of Elasticity, E 29500 ksi
 Yield Strength, Fy 64.4 ksi
 Tensile Strength, Fu 76.5 ksi
 Warping Constant Override, Cw 0 in⁶
 Torsion Constant Override, J 0 in⁴

Z-Section, Thickness 0.059 in
 Placement of Part from Origin:
 X to center of gravity 0 in
 Y to center of gravity 0 in

Outside dimensions, Open shape

	Length (in)	Angle (deg)	Radius (in)	Web	k Coef.	Hole Size (in)	Distance (in)
1	0.9410	-50.000	0.25000	None	0.000	0.0000	0.4705
2	2.1250	0.000	0.25000	Single	0.000	0.0000	1.0625
3	8.0000	90.000	0.25000	Zee	0.000	0.0000	4.0000
4	2.3750	0.000	0.25000	Single	0.000	0.0000	1.1875
5	0.9410	-50.000	0.25000	None	0.000	0.0000	0.4705

Fully Braced Strength - 2001 AISI Specification - US (ASD)

Compression		Positive Moment		Positive Moment	
Pao	16155 lb	Maxo	66.299 k-in	Mayo	13.003 k-in
Ae	0.45154 in ²	Ixe	7.1238 in ⁴	Iye	0.9958 in ⁴
		Sxe(t)	1.7192 in ³	Sye(l)	0.3692 in ³
		Sxe(b)	1.8473 in ³	Sye(r)	0.3372 in ³
		Negative Moment		Negative Moment	
		Maxo	65.077 k-in	Mayo	13.819 k-in
		Ixe	7.2036 in ⁴	Iye	1.0217 in ⁴
		Sxe(t)	1.9305 in ³	Sye(l)	0.3650 in ³
		Sxe(b)	1.6876 in ³	Sye(r)	0.3584 in ³
Tension					
Ta	31449 lb				
Shear					
Vay	2476 lb				
Vax	5121 lb				

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ISO 9001-2000

CERTIFICATE OF TEST

ATTENTION : BRANDON JASEK
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HUMBLE, TX 77338

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Houston, TX 77064
281/469-2609

LAB# : W0901579

DATE : 02/12/09 12:11:35
PO NO :13-0459T-08
SPECIMEN :14REGU1

TEST DATA

REDUCED SECTION TENSILE

UTS PSI	YS.2%PSI	%EL	%RA	WIDTH	THICK	AREA IN.
76,700	62,200	17.80	52.00	0.503	0.059	0.030


MTEC Representative

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SERVICES

ISO 9001-2000

CERTIFICATE OF TEST

ATTENTION : BRANDON JASEK
CUSTOMER : FORCE ENGINEERING & TESTING INC.
19530 RAMBLEWOOD DR
HUMBLE, TX 77338

8676 TAUB ROAD
Houston, TX 77064
281/469-2609

LAB# : W0901580

DATE : 02/12/09 12:12:18
PO NO :13-0459T-08
SPECIMEN :14REGU2

TEST DATA

REDUCED SECTION TENSILE

UTS PSI	YS.2%PSI	%EL	%RA	WIDTH	THICK	AREA IN.
75,600	64,800	19.10	65.50	0.500	0.059	0.030


MTEC Representative

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SERVICES

ISO 9001-2000

CERTIFICATE OF TEST

ATTENTION : BRANDON JASEK
CUSTOMER : FORCE ENGINEERING & TESTING INC.
19530 RAMBLEWOOD DR
HUMBLE, TX 77338

8676 TAUB ROAD
Houston, TX 77064
281/469-2609

LAB# : W0901581

DATE : 02/12/09 12:13:21
PO NO :13-0459T-08
SPECIMEN :14REGU3

TEST DATA

REDUCED SECTION TENSILE

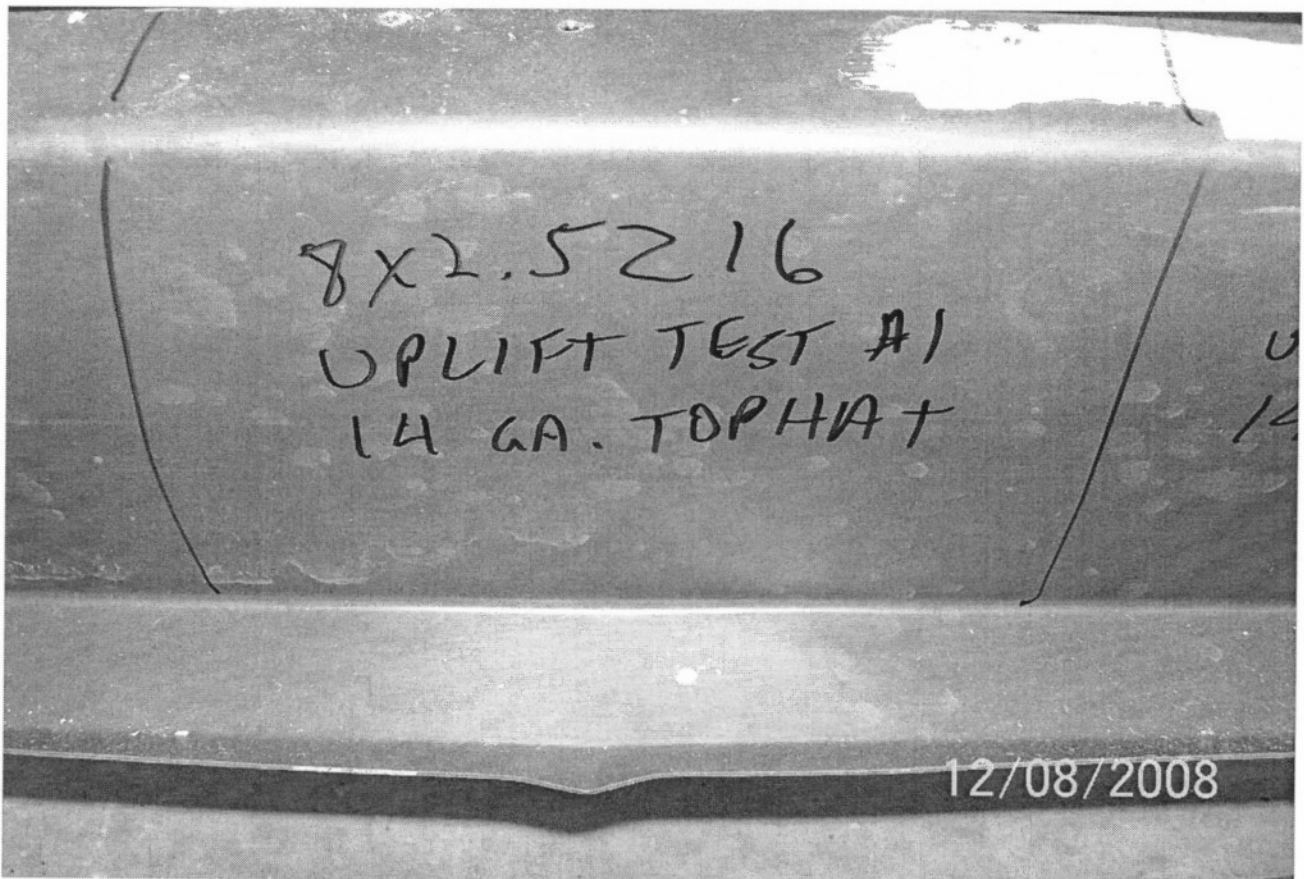
UTS PSI	YS.2%PSI	%EL	%RA	WIDTH	THICK	AREA IN.
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MTEC Representative

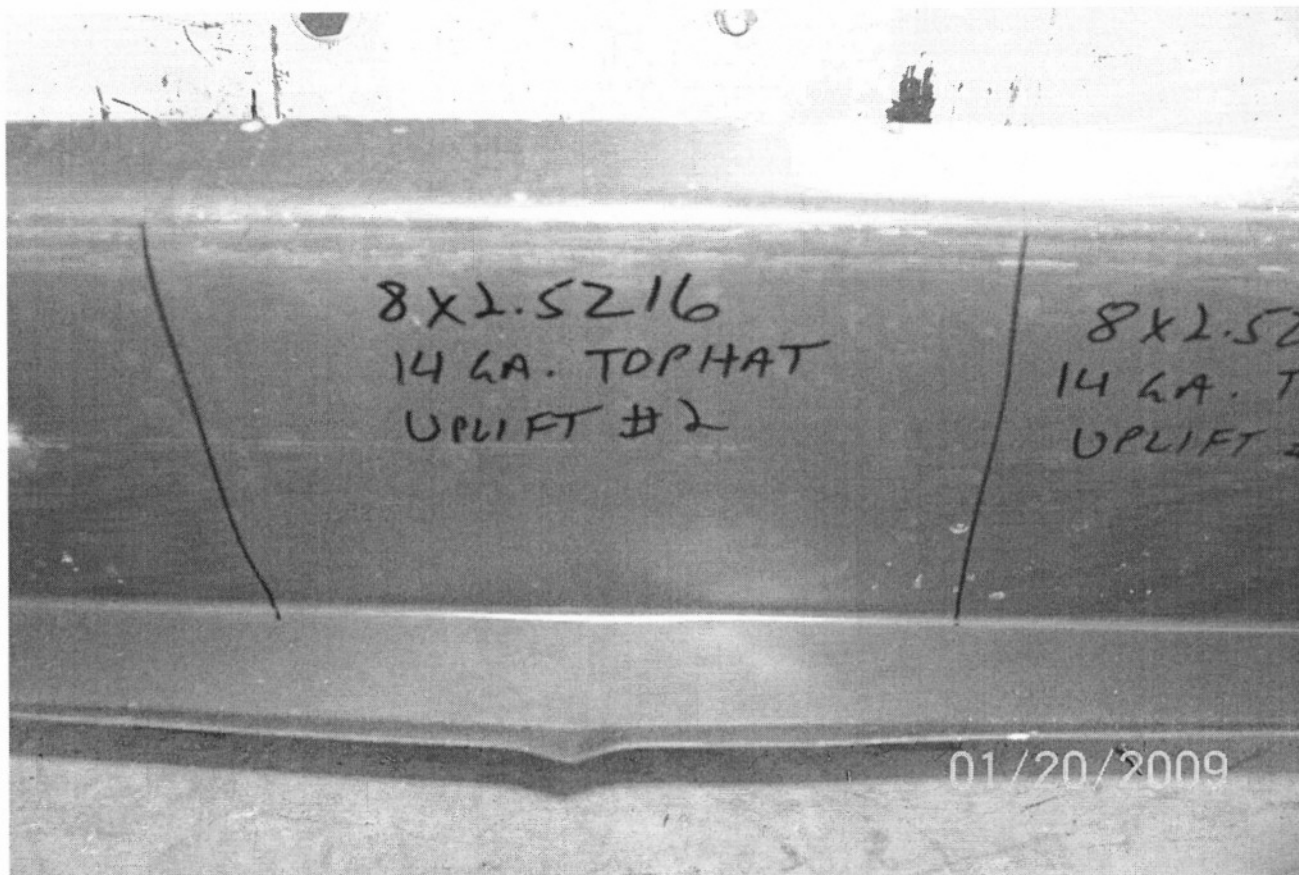
Photos



TYPICAL TEST SET UP



TEST G FAILURE



TEST H FAILURE



TEST I FAILURE